


# SIMULATING THE SPENT FUEL RECIPE OF A SODIUM-COOLED FAST REACTOR

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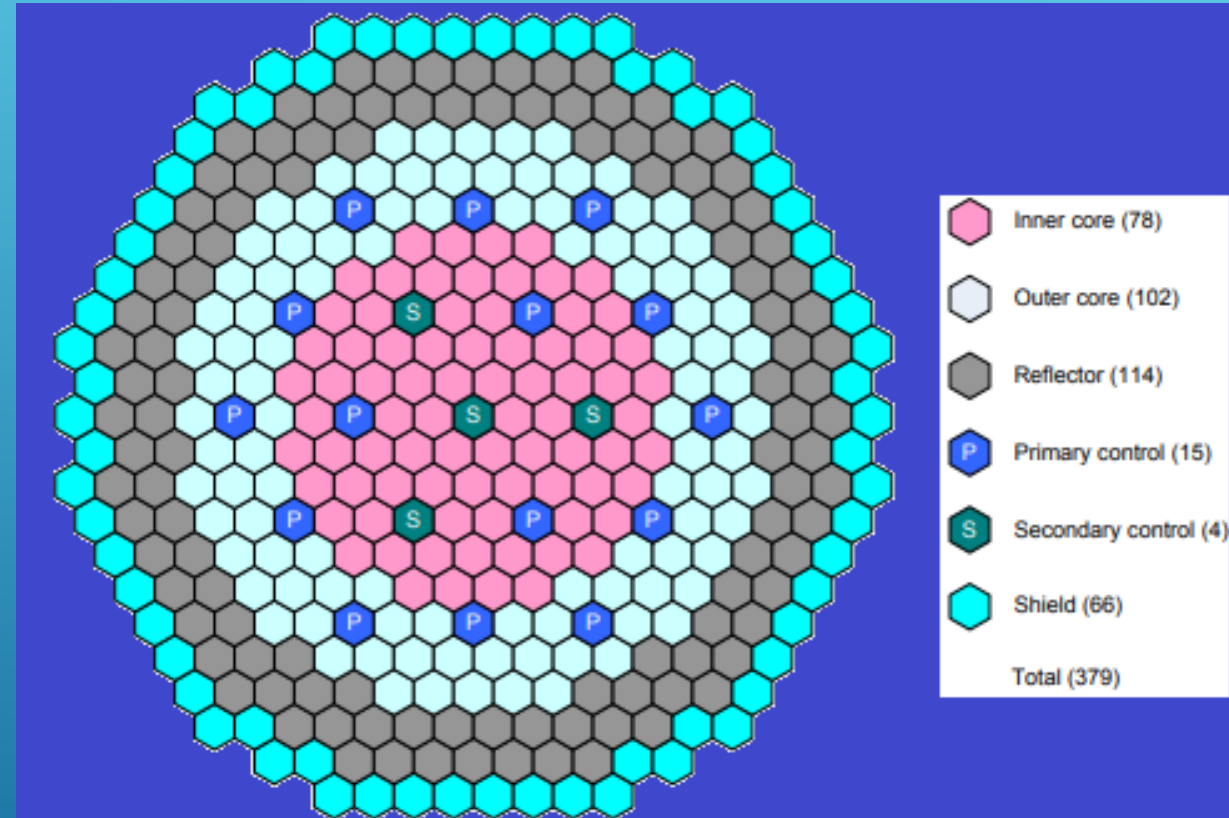
A decorative graphic consisting of several parallel white lines of varying lengths, all oriented diagonally from the bottom-left towards the top-right, located in the lower right quadrant of the slide.

# MOTIVATION

- ▶ Climate Change
  - ▶ Peak Oil
  - ▶ Gen-IV Reactor
    - ▶ Transition Scenarios
  - ▶ Cyclus
    - ▶ RAVEN and Reduced-Order Models
- 
- A decorative graphic consisting of several parallel white lines of varying lengths, slanted upwards from left to right, located in the bottom right corner of the slide.


# REACTOR BENCHMARK

- ▶ OECD Benchmark
- ▶ Octagonal Geometry
- ▶ 379 Hexagonal Subassemblies
- ▶ 5 Layers of Fuel
- ▶ No Blanket
- ▶ 1-GWth
- ▶ Circular Pins
- ▶ Pin Pitch =  $P/n \tan(\pi/6) = 9.38021/n$



	Unit	Value
Reactor power	MW-thermal	1000.0
Coolant temperature	°C	432.5
Average core structural temperature	°C	432.5
Average fuel temperature	°C	534.0

# FRESH FUEL COMPOSITION

- ▶ Metal Fuel Form
  - ▶ 24 isotopes including Uranium, Neptunium, Plutonium, Americium, Californium, Zirconium, and Molybdenum
  - ▶ 5 Vertical “Layers” of Fuel
  - ▶ Inner and Outer Core
  - ▶ Same Isotopes at Different Abundances in Inner/Outer Core and Different Layers
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# ▶ INNER CORE FUEL COMPOSITION

Nuclide	Upper boundary from active core bottom (cm)				
	17.16	34.33	51.49	68.66	85.82
<sup>234</sup> U	1.1369E-06	1.0856E-06	1.0727E-06	1.1028E-06	1.1759E-06
<sup>235</sup> U	3.0421E-05	2.9338E-05	2.8961E-05	3.0070E-05	3.2571E-05
<sup>236</sup> U	2.4896E-06	2.5117E-06	2.5536E-06	2.3779E-06	2.0226E-06
<sup>238</sup> U	1.9613E-02	1.9474E-02	1.9433E-02	1.9550E-02	1.9801E-02
<sup>237</sup> Np	4.6686E-05	4.6962E-05	4.6782E-05	4.7603E-05	4.8895E-05
<sup>236</sup> Pu	4.9700E-10	5.5883E-10	5.6701E-10	5.5075E-10	4.8775E-10
<sup>238</sup> Pu	1.1695E-04	1.1284E-04	1.1196E-04	1.1370E-04	1.1829E-04
<sup>239</sup> Pu	2.2076E-03	2.1814E-03	2.1754E-03	2.1813E-03	2.2011E-03
<sup>240</sup> Pu	1.3244E-03	1.2955E-03	1.2902E-03	1.2986E-03	1.3248E-03
<sup>241</sup> Pu	1.9375E-04	1.8610E-04	1.8518E-04	1.8537E-04	1.8845E-04
<sup>242</sup> Pu	2.9277E-04	2.8911E-04	2.8818E-04	2.9038E-04	2.9569E-04
<sup>241</sup> Am	1.0791E-04	1.0465E-04	1.0353E-04	1.0686E-04	1.1421E-04
<sup>242m</sup> Am	9.2989E-06	9.0848E-06	9.0224E-06	9.1756E-06	9.4890E-06
<sup>243</sup> Am	1.0017E-04	9.8324E-05	9.7993E-05	9.8630E-05	1.0032E-04
<sup>242</sup> Cm	5.6250E-06	5.8208E-06	5.9476E-06	5.4901E-06	4.5416E-06
<sup>243</sup> Cm	5.4321E-07	5.0246E-07	5.0136E-07	4.8876E-07	4.8480E-07
<sup>244</sup> Cm	6.7240E-05	6.5722E-05	6.5622E-05	6.5349E-05	6.5394E-05
<sup>245</sup> Cm	1.7397E-05	1.6743E-05	1.6663E-05	1.6696E-05	1.7026E-05
<sup>246</sup> Cm	9.2285E-06	9.1426E-06	9.1307E-06	9.1364E-06	9.1805E-06
Zr	7.2802E-03	7.2802E-03	7.2802E-03	7.2802E-03	7.2802E-03
<sup>a</sup> Mo	9.2873E-04	1.1464E-03	1.2031E-03	1.0625E-03	7.4065E-04


a) representative for pseudo fission product

# ▶ OUTER CORE FUEL COMPOSITION

Nuclide	Upper boundary from active core bottom (cm)				
	17.16	34.33	51.49	68.66	85.82
<sup>234</sup> U	1.6317E-06	1.5766E-06	1.5638E-06	1.5894E-06	1.6552E-06
<sup>235</sup> U	3.0822E-05	2.9870E-05	2.9561E-05	3.0391E-05	3.2250E-05
<sup>236</sup> U	1.7881E-06	1.8534E-06	1.8941E-06	1.7528E-06	1.4710E-06
<sup>238</sup> U	1.8244E-02	1.8144E-02	1.8115E-02	1.8191E-02	1.8359E-02
<sup>237</sup> Np	9.8244E-05	9.7300E-05	9.6775E-05	9.8481E-05	1.0175E-04
<sup>236</sup> Pu	7.1175E-10	8.2505E-10	8.4282E-10	8.0703E-10	6.8053E-10
<sup>238</sup> Pu	1.6436E-04	1.6026E-04	1.5949E-04	1.6063E-04	1.6416E-04
<sup>239</sup> Pu	2.8147E-03	2.7664E-03	2.7538E-03	2.7786E-03	2.8416E-03
<sup>240</sup> Pu	1.7467E-03	1.7191E-03	1.7135E-03	1.7231E-03	1.7508E-03
<sup>241</sup> Pu	2.8976E-04	2.8138E-04	2.8012E-04	2.8135E-04	2.8697E-04
<sup>242</sup> Pu	4.0754E-04	4.0412E-04	4.0321E-04	4.0530E-04	4.1028E-04
<sup>241</sup> Am	1.8607E-04	1.8127E-04	1.7970E-04	1.8397E-04	1.9339E-04
<sup>242m</sup> Am	1.2185E-05	1.2045E-05	1.2021E-05	1.2039E-05	1.2064E-05
<sup>243</sup> Am	1.3234E-04	1.3019E-04	1.2985E-04	1.3036E-04	1.3206E-04
<sup>242</sup> Cm	6.4688E-06	6.8630E-06	7.0553E-06	6.4446E-06	5.1976E-06
<sup>243</sup> Cm	6.3471E-07	6.0893E-07	6.0901E-07	5.9753E-07	5.9372E-07
<sup>244</sup> Cm	8.0107E-05	7.8889E-05	7.8847E-05	7.8479E-05	7.8359E-05
<sup>245</sup> Cm	2.0200E-05	1.9678E-05	1.9613E-05	1.9635E-05	1.9913E-05
<sup>246</sup> Cm	1.0443E-05	1.0371E-05	1.0361E-05	1.0367E-05	1.0410E-05
Zr	7.2802E-03	7.2802E-03	7.2802E-03	7.2802E-03	7.2802E-03
<sup>a)</sup> Mo	8.1524E-04	1.0174E-03	1.0697E-03	9.4870E-04	6.6172E-04

a) representative for pseudo fission product

# SERPENT2

- ▶ Monte-Carlo based Simulation Software
  - ▶ Universe-Based Constructive Solid Geometry
    - ▶ Pin < Subassembly < Lattice
  - ▶ Continuous-Energy
  - ▶ Developed at VTT Technical Research Centre of Finland
  - ▶ Plain text Input File
    - ▶ Geometry
    - ▶ Material
    - ▶ Simulation Parameters
  - ▶ Plain text and Image Output
- 

# MATERIAL CARDS

- ▶ Provide Alias and ZAID for Each Material In Reactor
- ▶ Provide Number Densities of Isotopes
- ▶ ACE, NFY, DEC Libraries for Material Properties
  - ▶ Courtesy of ARFC

```
% --- Fuel in inner core bottom (composition in atom density) (atoms/barn-cm):  
mat in-fuel-bot sum burn 1  
92234.09c 1.1369E-06 %U-234  
92235.09c 3.0421E-05 %U-235  
92236.09c 2.4896E-06 %U-236  
92238.09c 1.9613E-02 %U-238  
93237.09c 4.6686E-05 %Np-237  
94236.09c 4.9700E-10 %Pu-236  
94239.09c 1.1695E-04 %Pu-238  
94239.09c 2.2076E-03 %Pu-239  
94240.09c 1.3244E-03 %Pu-240  
94241.09c 1.9375E-04 %Pu-241  
94242.09c 2.9277E-04 %Pu-242  
95241.09c 1.0791E-04 %Am-241  
95342.09c 9.2989E-06 %Am-242m  
95243.09c 1.0017E-04 %Am-243  
96242.09c 5.6250E-06 %Cm-242  
96243.09c 5.4321E-07 %Cm-243  
96244.09c 6.7240E-05 %Cm-244  
96245.09c 1.7397E-05 %Cm-245  
96246.09c 9.2285E-06 %Cm-246  
40000.09c 7.2802E-03 %Natural Zr  
42000.09c 9.2873E-04 %a-Mo fission pseudo product
```



# PIN CARDS

- ▶ A Universe of Coaxial Cylinders of Homogeneous Material
- ▶ Provide Alias of Fill Material and Outer Radius
- ▶ Outermost Region is Coolant

```
pin 10 %coolant  
cool
```

```
pin 11 %inner core bottom  
in-fuel-bot 0.3236  
clad 0.3857  
cool
```

```
pin 12 %outer core bottom  
out-fuel-bot 0.3236  
clad 0.3857  
cool
```

```
pin 13 %reflector  
refl 0.7557  
cool
```

```
pin 14 %shielding  
absonat 1.4277  
clad 1.6794  
cool
```

```
pin 15 %control  
abso 2.2890  
clad 2.3606  
cool
```

# GEOMETRY CODE

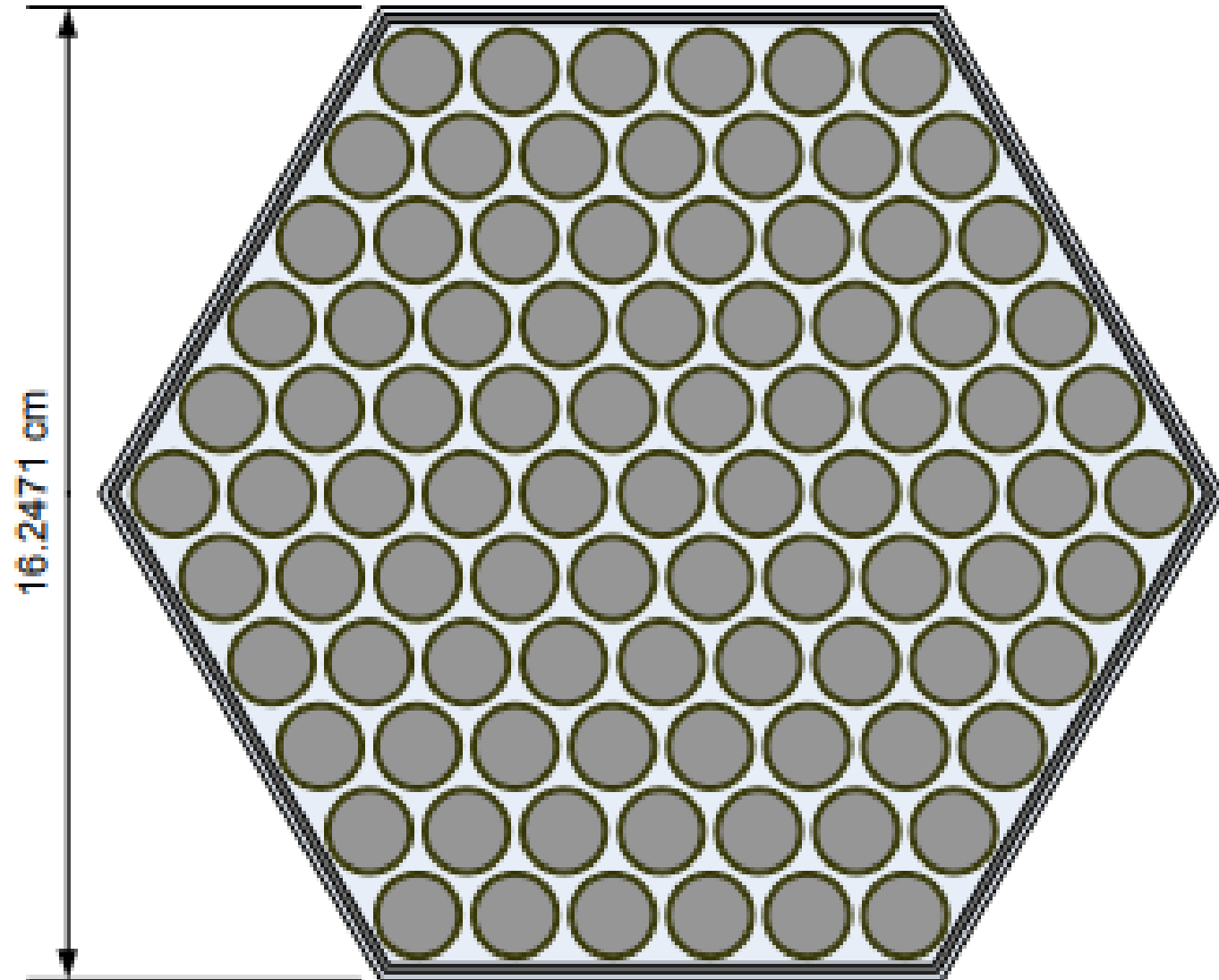
- ▶ Pictures of Benchmark Schematic next to Code to Model that Region of the Reactor





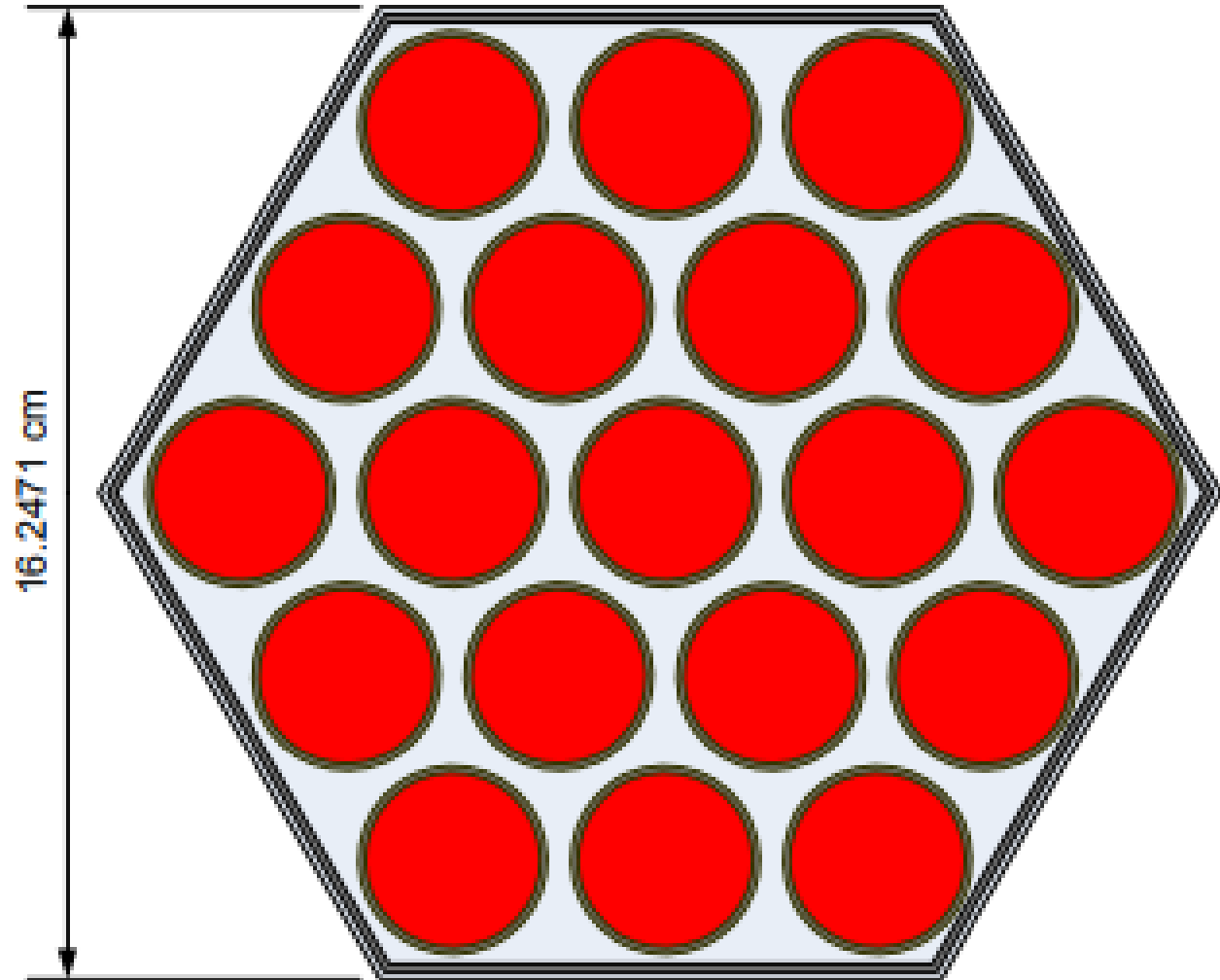
# REFLECTOR SUBASSEMBLY

```
lat 23 3 0 0 13 13 1.56337 %reflector subassembly pin pitch = 1.9 cm
10 10 10 10 10 10 10 10 10 10 10 10 10
10 10 10 10 10 10 13 13 13 13 13 13 10
10 10 10 10 10 13 13 13 13 13 13 13 10
10 10 10 13 13 13 13 13 13 13 13 13 10
10 10 13 13 13 13 13 13 13 13 13 13 10
10 13 13 13 13 13 13 13 13 13 13 13 10
10 13 13 13 13 13 13 13 13 13 13 10 10
10 13 13 13 13 13 13 13 13 13 10 10 10
10 13 13 13 13 13 13 13 13 10 10 10 10
10 13 13 13 13 13 13 10 10 10 10 10 10
10 10 10 10 10 10 10 10 10 10 10 10 10
```



# SHIELD SUBASSEMBLY

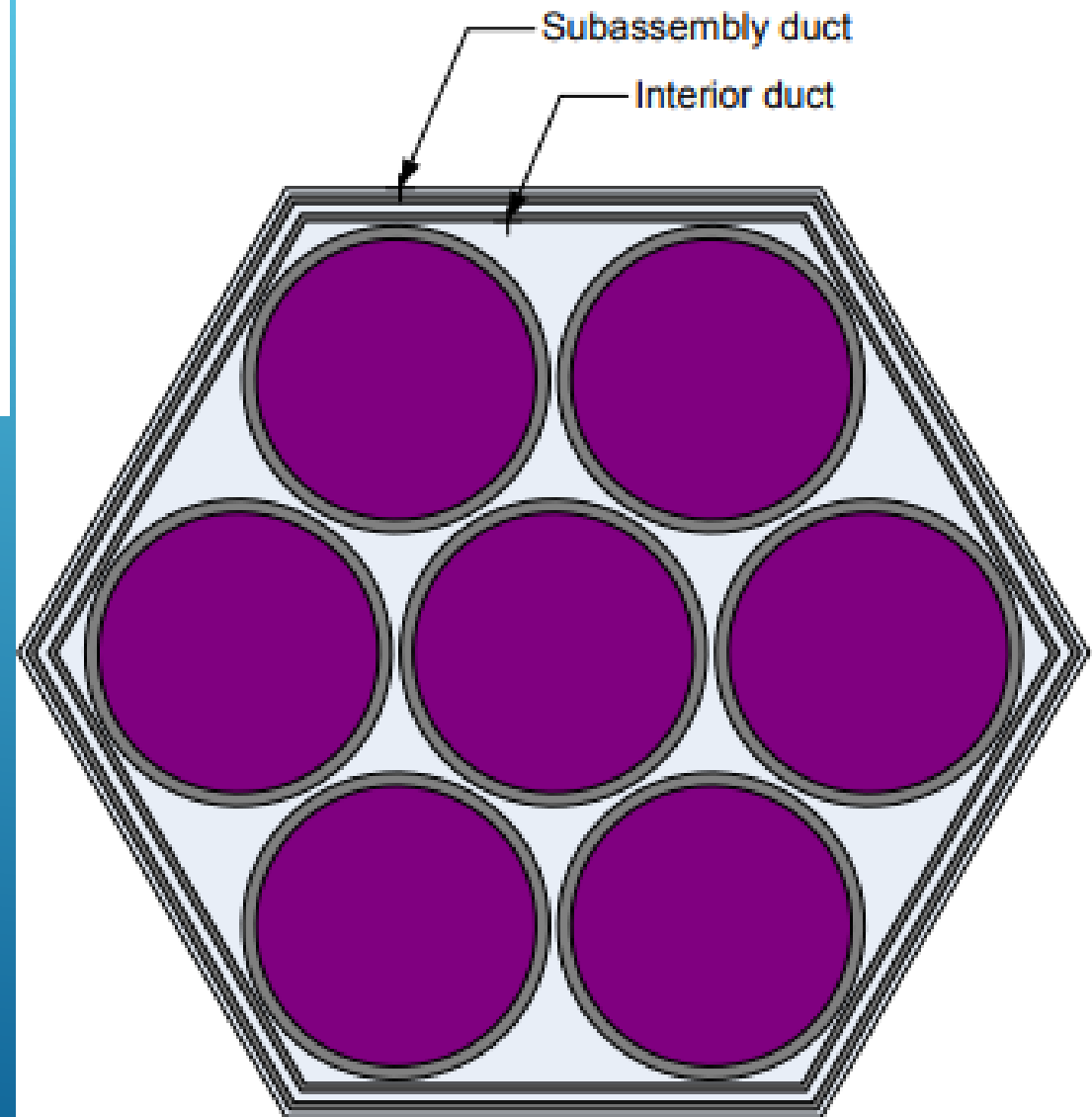
```
lat 24 3 0 0 7 7 3.12674 % pin pitch = 4.7cm
10 10 10 10 10 10 10
10 10 10 14 14 14 10
 10 10 14 14 14 14 10
   10 14 14 14 14 14 10
    10 14 14 14 14 10 10
     10 14 14 14 10 10 10
      10 10 10 10 10 10 10
```



Section A-A

# CONTROL ROD SUBASSEMBLY

```
lat 25 3 0 0 5 5 4.690105 %pin pitch = 1.9cm  
10 10 10 10 10  
10 10 15 15 10  
10 15 15 15 10  
10 15 15 10 10  
10 10 10 10 10
```



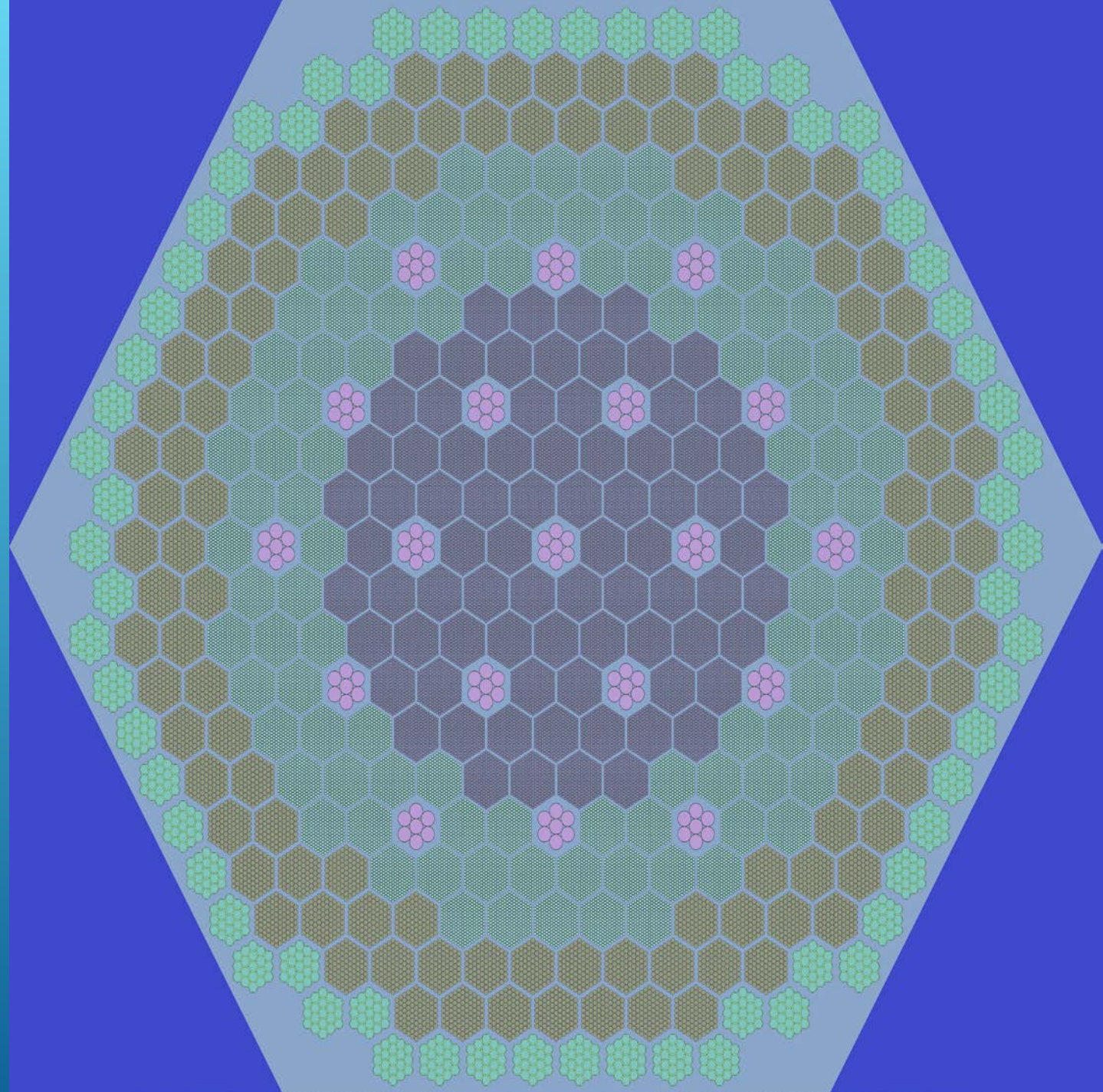






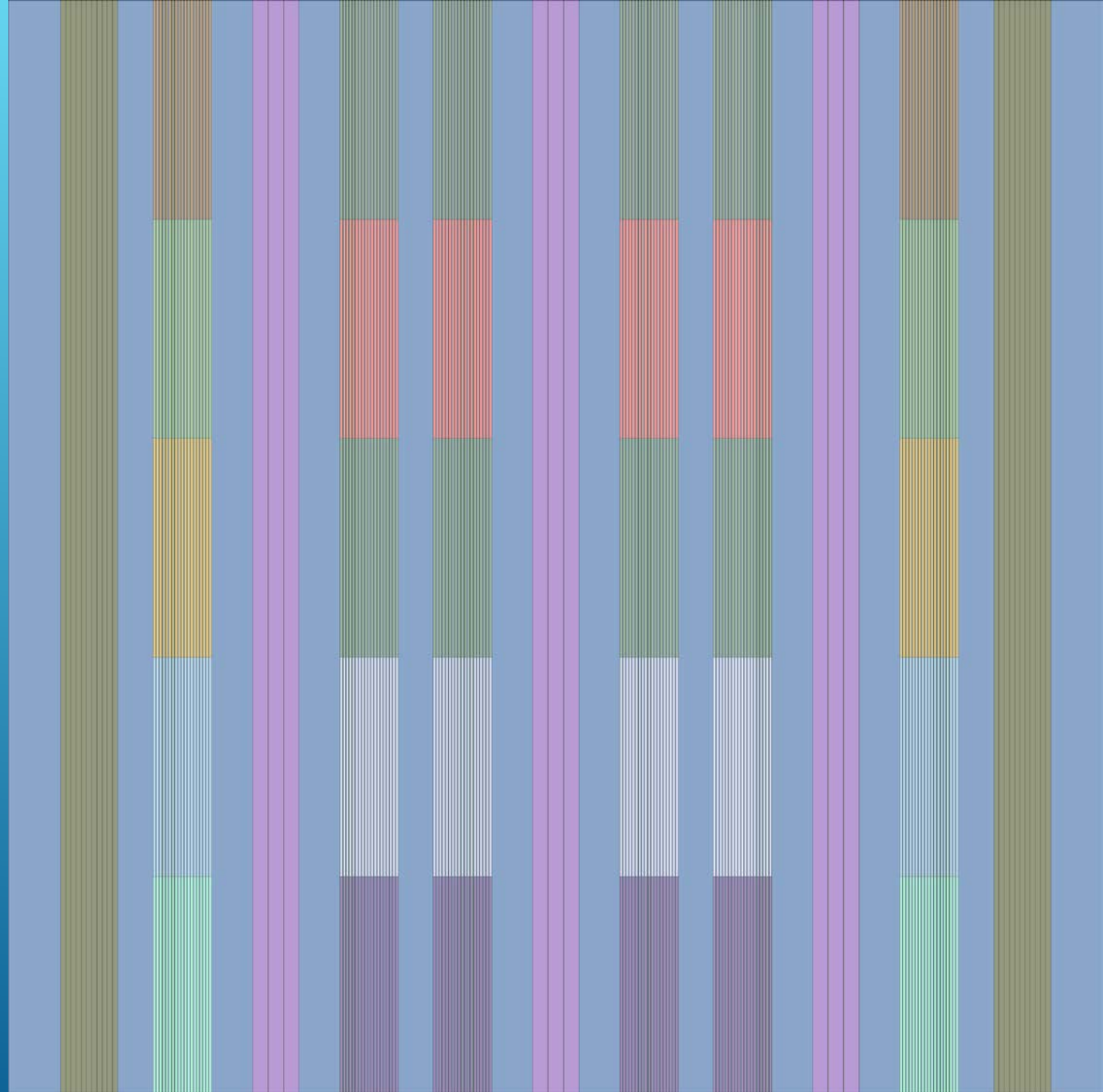
# GEOMETRY PLOT

- ▶ View along Z-Axis
- ▶ Different Color Corresponds to Different Pin Universe



# GEOMETRY PLOT

- ▶ View from Y-axis
- ▶ Five Layers of Fuel



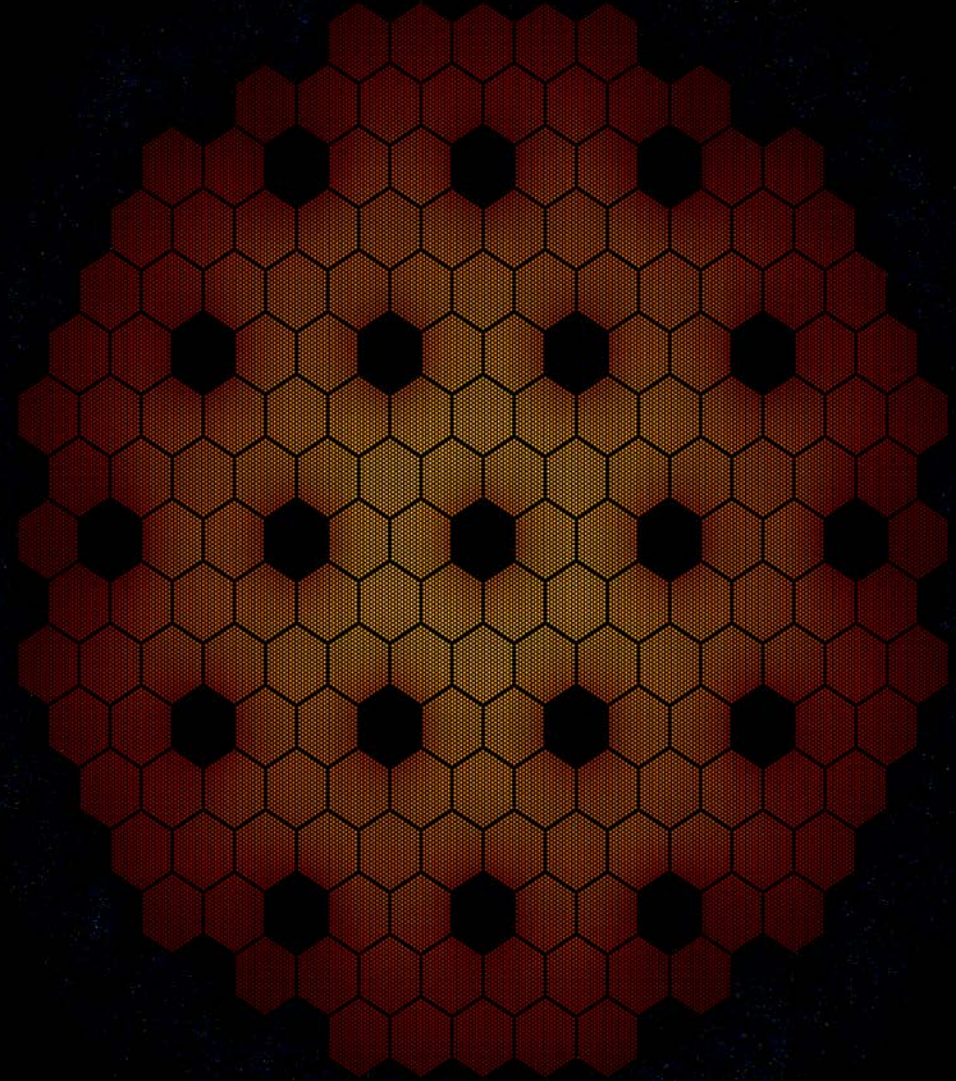
# BURNUP PLOT - BEFORE

- ▶ Color Indicates Flux
- ▶ Absorbers Doing A Good Job

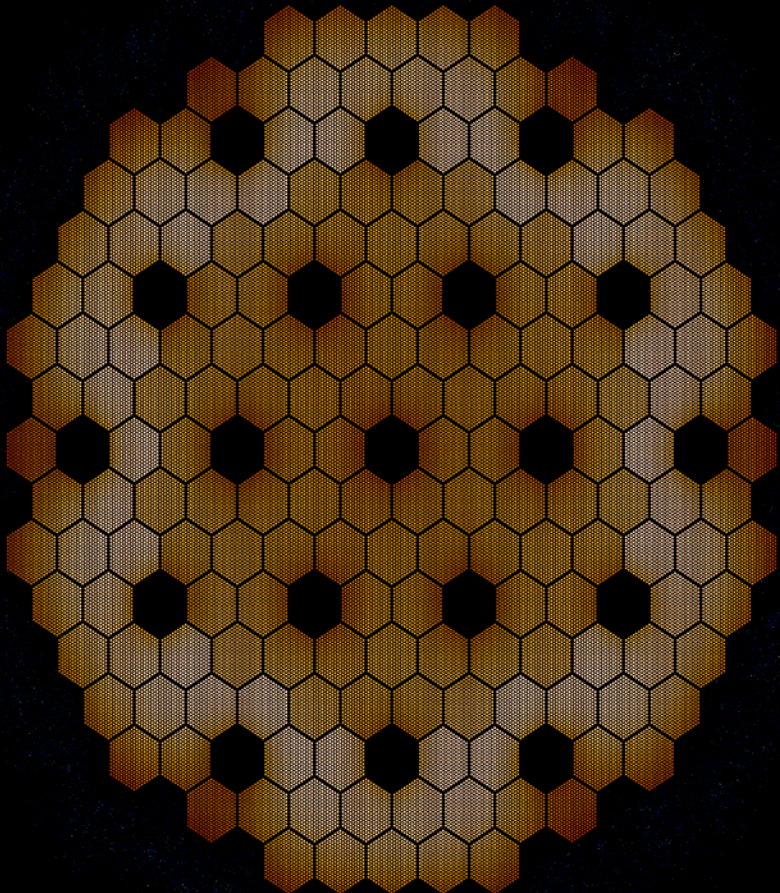


# BURNUP PLOT - AFTER

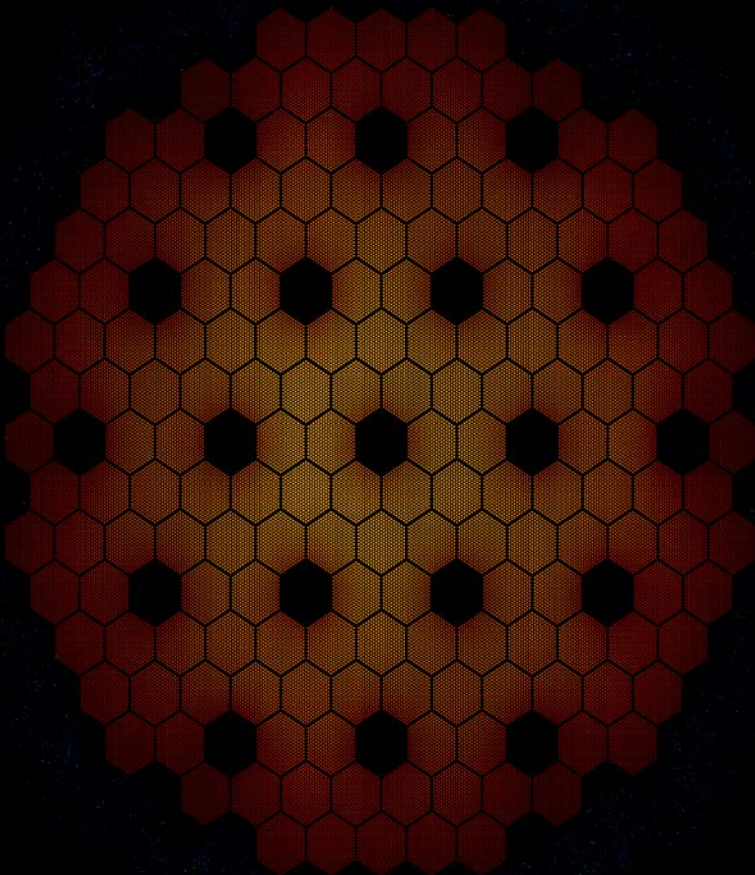
- ▶ One Year Of Operation
- ▶ Dimmer Plot Indicates Refueling Is Needed




BEFORE



AFTER



# USED FUEL COMPOSITION

- ▶ Over 2000 different nuclides
  - ▶ “Recipe” Input for Cyclus
  - ▶ Reduced Order Model for Raven
- 

# REFERENCES & ACKNOWLEDGEMENTS

- ▶ 1) OECD-NEA (February 2016). Benchmark for Neutronic Analysis of Sodium-cooled Fast Reactor Cores with Various Fuel Types and Core Sizes, Retrieved From: [www.oecd-nea.org](http://www.oecd-nea.org)
  - ▶ 2) J. Leppänen (June 18, 2015), Serpent – a Continuous-energy Monte Carlo Reactor Physics Burnup Calculation Code. VTT Technical Research Centre of Finland. Retrieved From: [montecarlo.vtt.fi](http://montecarlo.vtt.fi)
  - ▶ Special Thanks to Professor Katy Huff, Andrei Rykhlevskii, University of Illinois, and The Department of NPRE
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